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(54) Title: CARDABLE HYDROPHOBIC POLYOLEFIN FIBRES

(57) Abstract

A method for producing cardable, hydrophobic polyolefin-based staple fibres, comprising applying to spun filaments a first spin finish comprising an antistatic agent, in particular a neutralized phosphoric acid ester, stretching the filaments, applying to the stretched filaments a second spin finish in the form of a dispersion comprising: i) an antistatic agent, ii) a natural or synthetic hydrocarbon wax with a melting point in the range of 40-120 °C, or a wax mixture comprising at least one such hydrocarbon wax and having a melting point in the range of 40-150 °C, and optionally iii) a polydiorganosiloxane, crimping the filaments, drying the filaments, and cutting the filaments to obtain staple fibres, as well as fibres produced by the method and nonwovens prepared from the fibres. The invention allows the production of fibres that have controlled friction and hydrophobic properties and that can be carded at high speeds to result in nonwovens having excellent hydrophobic characteristics.

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## CARDABLE HYDROPHOBIC POLYOLEFIN FIBRES

## FIELD OF THE INVENTION

The present invention relates to cardable and thermobondable polyolefin-based synthetic fibres treated with hydrophobic

5 spin finishes comprising an antistatic agent and a hydrophobic agent, a method for producing the fibres, and nonwoven products prepared from the fibres.

The fibres, which have the advantage of being able to be carded at high speeds, are particularly suitable for use in  
10 the preparation of thermally bonded hydrophobic nonwoven fabrics in which a dry, water repellent surface which can function as a liquid barrier is desired, e.g. for disposable diapers and feminine hygienic products. The fibres are also suitable for the preparation of thermally bonded nonwoven  
15 fabrics for medical use in which a dry, water repellent surface is desired in order to reduce bacterial penetration, for example medical gowns and drapes.

## BACKGROUND OF THE INVENTION

A number of polyolefin-based hydrophobic synthetic fibres are known, for example hydrophobic textile fibres with dirt and stain resistant properties. However, such fibres generally contain cationic antistatic agents (for example alkylammonium salts, condensation products of fatty acids and ethanol amines, and alkylimidazolinium salts). Such cationic  
25 antistatic agents are undesirable or unsuitable for personal hygiene and medical products for toxicological reasons, since they exhibit skin irritating properties due to their non-neutral pH and possible release of di- or tri-ethanolamine, which is suspected of causing allergic reactions. Attempts to  
30 produce cardable and thermobondable synthetic fibres for hygienic or medical use have not been entirely successful. In particular, fibres having good cardability properties together with satisfactory hydrophobic properties have not

been obtainable. This is particularly important for the many applications in which it is desired that hydrophobic fibres may be carded using high carding speeds.

Hygienic products such as disposable diapers, sanitary  
5 napkins and adult incontinence pads generally have barriers through which fluids absorbed by the absorbent core are not able to penetrate, e.g. in the form of side guards, other structural elements, or as back sheet material opposite to the skin. Such barriers may comprise a nonwoven material  
10 prepared from hydrophobic staple fibres or a spun-bonded material prepared directly from a hydrophobic polymer. However, spun-bonded materials are very flat and film-like, and do not have the soft, uniform, textile-like comfort that one finds in nonwovens. Spun-bonded fabrics are therefore not  
15 the optimal choice for liquid barriers designed to be in contact with the skin of the user. As for nonwovens prepared from staple fibres, these tend not to be sufficiently hydrophobic for such liquid barriers, due to the fact that during the spinning process, the fibres are treated with a  
20 "spin finish" which facilitates the spinning process by lubricating the fibres and making them antistatic. However, as a result of the spin finish treatment, the fibres become somewhat hydrophilic, which in the present context is undesirable. On the other hand, fibres with the desired  
25 degree of hydrophobicity have not had optimum antistatic properties, and have therefore not been truly cardable, and certainly not at the high carding speeds typically used for carding of hydrophilic fibres.

US 4,938,832 discloses a method for preparing hydrophobic  
30 polyolefin-containing fibres or filaments in which spun fibres or filaments are treated with a first modifier composition containing 70-100% by weight of at least one neutralized phosphoric acid ester containing a lower alkyl group and up to 30% by weight of at least one polysiloxane  
35 with hydrophobic end groups, followed by treatment with a second modifier composition containing 70-100% by weight of

the polysiloxane and up to 30% by weight of the neutralized phosphoric acid ester.

EP 0 486 158 A2 discloses a somewhat similar method for preparing hydrophobic polyolefin-containing fibres or filaments, in which spun fibres or filaments are treated with a first modifier composition containing 0-40% by weight of at least one neutralized phosphoric acid ester containing a lower alkyl group and 60-100% by weight of at least one polysiloxane with hydrophobic end groups, followed by treatment with a second modifier composition containing 50-100% by weight of the neutralized phosphoric acid ester and 0-50% by weight of the polysiloxane.

EP 0 516 412 A2 discloses a method for treating the surface of polyolefin-containing fibres to improve their lubricity and antistatic properties by applying a liquid lubricating finish containing an alkylated polyol, a water-soluble ester or polyester derived from the polyol or a glycol derived from the polyol. A polysiloxane and a neutralized phosphoric acid ester may also optionally be applied to the fibres.

EP 0 557 024 A1 discloses polyolefin fibres treated with an antistatic agent which is a neutralized phosphate salt, and optionally with a lubricant selected from mineral oils, paraffinic waxes, polyglycols and silicones, the fibres having an hydrostatic head value of at least 102 mm.

Japanese unexamined publication No. 3-69672/1991 (application No. 89/205380) discloses a treating agent for binder fibres containing 20-45% by weight of a C<sub>12</sub> or greater alkylphosphate, 20-70% by weight of a carboxyl-modified polyethylene wax with a MW of 1,000-10,000 and an acid value of 5-50 containing 5-30% of an emulsifier, 5-10% by weight of a higher alcohol, and 2-5% by weight of an optionally modified dimethylsilicone. The treating agent is applied to fibres before carding and is thus not a "spin finish" for use during production of the fibres. Carboxyl-modified waxes of

the type used according to this reference are relatively easy to emulsify, but they are disadvantageous for use in spin finishes for the production of hydrophobic fibres since they have a relatively high melting point and are somewhat 5 hydrophilic. The higher alcohol appears to be added to the treating agent in order to help reduce friction caused by the presence of a large amount of the high molecular weight carboxyl-modified wax.

Japanese patent publication No. 4-24463/1992 (application No. 10 86/84081) discloses polyester fibres coated with a spinning oil consisting of 40-85% by weight of at least one neutral oil with a melting point of 30-150°C, 5-30% by weight of a cationic surfactant, and the balance of an emulsifier. As discussed above, the use of cationic surfactants is, however, 15 undesirable in products designed for personal hygiene or medical use.

The fibres described in the above-mentioned publications all have various combinations and degrees of hydrophobic and antistatic properties. However, none of these fibres exhibit 20 the combination of optimum hydrophobic and antistatic properties desirable for the preparation, in particular by means of high-speed carding, of nonwovens with optimum strength and hydrophobic characteristics.

An object of the present invention is therefore to provide 25 hydrophobic thermobondable synthetic fibres, in particular for hygienic applications, with improved carding properties and which can be used to prepare nonwovens showing superior strength. A further object of the present invention is the provision of a method by which the hydrophobic properties and 30 the fibre/fibre and fibre/metal friction properties of spun fibres may be controlled, thereby allowing optimum fibre distribution and strength in nonwovens containing the fibres.

## BRIEF DISCLOSURE OF THE INVENTION

In one aspect, the present invention relates to a method for producing cardable, hydrophobic polyolefin-based staple fibres, the method comprising the following steps:

- 5    a. applying to spun filaments a first spin finish comprising an antistatic agent,
- b. stretching the filaments,
- c. applying to the stretched filaments a second spin finish in the form of a dispersion comprising i) an antistatic agent, ii) a natural or synthetic hydrocarbon wax with a melting point in the range of 40-120°C, or a wax mixture comprising at least one such hydrocarbon wax and having a melting point in the range of 40-120°C, and optionally iii) a polydiorganosiloxane,
- 10    d. crimping the filaments,
- e. drying the filaments, and
- f. cutting the filaments to obtain staple fibres.

In a second aspect, the present invention relates to a fibre produced by the above method, the fibre being a texturized, cardable, polyolefin-based fibre carrying, at its surface, 0.10-0.50% by weight of the fibre of an antistatic agent, 0.10-0.35% by weight of the fibre of a natural or synthetic hydrocarbon wax with a melting point in the range of 40-120°C or of a wax mixture comprising at least one such hydrocarbon wax and having a melting point in the range of 40-120°C, 0-0.25% by weight of the fibre of a polydialkylsiloxane, and 0.001-0.10% by weight of the fibre of an emulsifier.

In a further aspect, the invention relates to a hydrophobic nonwoven material comprising the fibres of the invention.

- 30    In a still further aspect, the invention relates to a method for preparing a hydrophobic nonwoven material, comprising processing the fibres of the invention to obtain a web for bonding, and thermobonding the resulting web to obtain the hydrophobic nonwoven material.

The fibres of the present invention have been found to have superior antistatic properties compared to known hydrophobic fibres and can therefore be carded at high carding speeds comparable to carding speeds typically used for hydrophilic 5 staple fibres. The fibres' suitability for high-speed carding is also due to their controlled fibre/fibre and fibre/metal friction properties obtained by varying the composition of the second spin finish. It has furthermore been found that webs prepared from the fibres have a uniform distribution of 10 the fibres in both the machine direction and the transverse direction, and that when these webs are thermobonded by calender bonding nonwovens with improved strength and excellent hydrophobicity are obtained.

15 Fibres prepared according to the present invention may be either white (unpigmented) or coloured (pigmented) fibres.

#### DETAILED DISCLOSURE OF THE INVENTION

The terms "polyolefin-based", "polypropylene-based" and "polyethylene-based" refer to the fact that the fibres of the present invention are produced from a polyolefin or a 20 copolymer thereof, including isotactic polypropylene homopolymers as well as random copolymers thereof with ethylene, 1-butene, 4-methyl-1-pentene, etc., and linear polyethylenes of different densities, such as high density polyethylene, low density polyethylene and linear low density 25 polyethylene. The melts used to produce the polyolefin-based fibres may also contain various conventional fibre additives, such as calcium stearate, antioxidants, and pigments, including whiteners and colourants such as TiO<sub>2</sub>, etc.

30 The hydrophobic fibres may be either monocomponent or bicomponent fibres, the latter being for example sheath-and-core type bicomponent fibres with the core being located either eccentrically (off-center) or concentrically (substantially in the center). Bicomponent fibres will typically have a core and sheath which comprise,

respectively, polypropylene/polyethylene, high density polyethylene/linear low density polyethylene, polypropylene random copolymer/polyethylene, or polypropylene/polypropylene random copolymer.

- 5 The spinning of the fibres is preferably accomplished using conventional melt spinning (also known as "long spinning"), in particular medium-speed conventional spinning.
- Conventional spinning involves a two-step process, the first step being the extrusion of the melts and the actual spinning 10 of the fibres, and the second step being the stretching of the spun fibres, in contrast to so-called "short spinning", which is a one-step process in which the fibres are both spun and stretched in a single operation.
- For spinning, the melted fibre components are led from their 15 respective extruders, through a distribution system, and passed through the holes of a spinnerette. The extruded melts are then led through a quenching duct, where they are cooled and solidified by a stream of air, and at the same time drawn into filaments, which are gathered into bundles of typically 20 several hundred filaments. The spinning speed after the quenching duct is typically at least about 200 m/min, more typically about 400-2500 m/min. After having solidified, the filaments are treated with the first spin finish by means of lick rollers.
- 25 Stretching in a long spin process is performed using so-called off-line stretching or off-line drawing, which, as mentioned above, takes place separately from the spinning process. The stretching process typically involves a series of hot rollers and a hot air oven, in which a number of 30 bundles of filaments are stretched simultaneously. The bundles of filaments pass first through one set of rollers, followed by passage through a hot air oven, and then passage through a second set of rollers. Both the hot rollers and the hot air oven typically have a temperature of about 50-140°C, 35 e.g. about 70-130°C, the temperature being chosen according

to the type of fibre, e.g. typically 115-135°C for polypropylene fibres, 95-105°C for polyethylene fibres, and 110-120°C for polypropylene/polyethylene bicomponent fibres. The speed of the second set of rollers is faster than the 5 speed of the first set, and the heated bundles of filaments are therefore stretched according to the ratio between the two speeds (called the stretch ratio or draw ratio). A second oven and a third set of rollers can also be used (two-stage stretching), with the third set of rollers having a higher 10 speed than the second set. In this case the stretch ratio is the ratio between the speed of the last and the first set of rollers. Similarly, additional sets of rollers and ovens may be used. The fibres of the present invention are typically stretched using a stretch ratio of from about 1.05:1 to about 15 6:1, e.g. from 1.05:1 to 2:1 for polypropylene fibres, from 2:1 to 4.5:1 for polyethylene fibres and polypropylene/polyethylene bicomponent fibres, resulting in an appropriate fineness, i.e. about 1-7 dtex, typically about 1.5-5 dtex, more typically about 1.6-3.4 dtex. After 20 stretching, the bundles of filaments are treated with the second spin finish by means of lick rollers.

Texturization (crimping) of the stretched fibres is performed in order to make the fibres suitable for carding by giving them a "wavy" form. An effective texturization, i.e. a 25 relatively large number of crimps in the fibres, allows for high processing speeds in the carding machine, typically at least about 80 m/min, such as at least 100 m/min, and in many cases at least 150 m/min or even 200 m/min or more, and thus a high productivity.

30 Crimping is typically carried out using a so-called stuffer box. The bundles of filaments are led by a pair of pressure rollers into a chamber in the stuffer box, where they become crimped due to the pressure that results from the fact that they are not drawn forward inside the chamber. The degree of 35 crimping can be controlled by the pressure of the rollers prior to the stuffer box, the pressure and temperature in the

chamber and the thickness of the bundle of filaments. As an alternative, the filaments can be air-texturized by passing them through a nozzle by means of a jet air stream.

The fibres of the present invention are typically texturized 5 to a level of about 5-15 crimps/cm, typically about 7-12 crimps/cm (the number of crimps being the number of bends in the fibres).

After the fibres have been crimped, e.g. in a stuffer box, they are typically fixed by heat treatment in order to reduce 10 tensions which may be present after the stretching and crimping processes, thereby making the texturization more permanent. Fixation and drying of the fibres may take place simultaneously, typically by leading the bundles of filaments from the stuffer box, e.g. via a conveyer belt, through a 15 hot-air oven. The temperature of the oven will depend on the composition of the fibres, but must obviously be below the melting point of the fibre polymer or (in the case of bicomponent fibres) the low melting component. During the fixation the fibres are subjected to a crystallization 20 process which "locks" the fibres in their crimped form, thereby making the texturization more permanent. The heat treatment also removes a certain amount of the water from the spin finishes. Of particular importance for the fibres of the present invention is the fact that the drying process allows 25 the wax component (together with any polydiorganosiloxane) to melt and become distributed uniformly on the surface of the filaments. The filaments are typically dried at a temperature in the range of 90-130°C, typically 95-125°C, depending on factors such as the type of fibre.

30 The fixed and dried bundles of filaments are then led to a cutter, where the fibres are cut to staple fibres of the desired length. Cutting is typically accomplished by passing the fibres over a wheel containing radially placed knives. The fibres are pressed against the knives by pressure from 35 rollers, and are thus cut to the desired length, which is

equal to the distance between the knives. The fibres of the present invention are typically cut to staple fibres of a length of about 18-150 mm, more typically about 25-100 mm, in particular about 30-65 mm, depending on the carding equipment 5 and the fineness of the fibres. A length of about 38-40 mm will thus often be suitable for a fibre with a fineness of about 2.2 dtex, while a length of 45-50 mm is often suitable for a 3.3 dtex fibre.

Quite generally, the main requirements for a spin finish for 10 spinning and stretching polymer fibres include the following:

1. It should contain an amount of antistatic agent which ensures that the fibres do not become electrically charged during the spinning and stretching process or during the carding process; anionic, cationic and non- 15 ionic antistatic agents are all employed in spin finishes (although cationic agents are for the reasons given above not preferred for the purposes of the present invention).
2. It should contain an amount of cohesion conferring agent sufficient to ensure that the filaments are held together 20 in bundles, allowing them to be processed without becoming entangled; neutral vegetable oils, long chained alcohols, ethers and esters, and non-ionic surface active agents are often employed for this purpose.
3. It should contain components which regulate both 25 fibre/fibre and fibre/metal friction during the production process, so that the filaments do not become worn or frayed during processing. In particular, fibre/metal friction during the spinning stage, fibre/metal friction against the stretch rollers, and fibre/fibre and fibre/metal friction in the crimper need to be regulated. Polyethyleneglycol fatty acid mono- or di-esters (in other words non-ionic surface active agents with a medium HLB (hydrophilic-lipophilic balance) value, e.g. a HLB 30 value of about 5-15) are often used; the cohesion

conferring agent mentioned above also has an influence on friction.

4. Water plus emulsifiers or surface active agents which keep the more or less lipophilic components in the aqueous solution are necessary. The solvent is normally water, since the anionic antistatic agent's effect otherwise tends to be greatly reduced, and furthermore the spin finish must be diluted in order to reduce viscosity and thereby achieve a sufficient wetting action
- 10 on the surface of the filaments.

Spin finishes also serve to regulate the fibre/fibre and fibre/metal friction during carding, and spin finishes used for spinning and stretching are generally adapted so that the fibres do not require any further processing before carding.

- 15 The present invention is based on spin finishes used in connection with both the spinning and stretching steps which fulfil the requirements listed above with regard to the content of antistatic agent, cohesion conferring agent, oil and water, as well as regulation of fibre/fibre and
- 20 fibre/metal friction. These spin finishes have the further advantage that they function as a processing aid during carding and thus provide the fibre/fibre and fibre/metal friction necessary to obtain sufficient carding of the fibres. As a result, a carding web with a uniform
- 25 distribution of the fibres is obtained, even when using relatively high carding speeds.

In the method of the present invention, the majority of the antistatic agent is applied in the spinning stage, and wax (as well as polydiorganosiloxane) are only applied in the

30 stretching stage. There are several reasons for choosing this approach. First of all, the use of wax during spinning results in problems for both spinning and stretching:

1. During spinning, the fibre/metal friction will be increased and part of the wax components will be deposited on various machine surfaces which are in contact with the filament bundles. Deposition of wax  
5 during spinning will also cause the bundle of filaments to be so sticky that it will partially stick to itself. If this happens, the fibre bundles will be difficult to take up out of the cans (boxes in which the bundles are stored until a number of bundles are ready to be  
10 stretched simultaneously) when they are to be stretched in the two-step process.
  2. During stretching, wax deposits will also be formed on the heated rollers and other machine parts that are in contact with the bundles. This is due to the fact that  
15 the bundle of filaments is heated during the stretching process. At elevated temperatures some of the water will evaporate from the applied spin finish, and a film of melted wax will easily be deposited on the rollers, etc. If this happens, friction between the bundles of  
20 filaments and the surface of the rollers will be reduced to a level below that which is necessary for maintenance of the drawing forces necessary to stretch the fibres. If, as a result, the fibres slide along the surface of the rollers, they will obviously not become stretched.
- 25 The use of silicone compounds during the spinning process would also give problems for both spinning and stretching:
1. During spinning, silicone would serve to reduce friction, so that the bundles of filaments would slide along the various drive rollers rather than being moved forward by  
30 the rollers. As a result, it would not be possible to pull the fibres out of the extruder at a predetermined and constant speed. This applies especially at the high speeds used in conventional spinning.

2. During stretching, silicone applied in the spinning stage would have the same negative effect as wax. Friction between the bundle of filaments and the stretch rollers would be reduced, resulting in the well-known slip problems caused by silicone.

By only applying a relatively hydrophobic antistatic agent and a very small amount of a cohesion conferring agent during the spinning stage (i.e. without wax or silicone in any significant amount), the above-mentioned processing problems 10 are avoided. The (relatively hydrophobic) antistatic agent should have sufficient antistatic properties, should contribute to the cohesion of the filaments, and should not have such a high molecular weight that it leads to problems with deposits on the machinery.

- 15 The second spin finish should contain a certain minimum amount of antistatic agent to provide the fibres with sufficient antistatic properties to be able to be carded without problems of static electric build-up. In addition, the second spin finish should contain a sufficient amount of 20 one or more hydrophobic components (wax and optional polydiorganosiloxane) so that the finished fibres as well as the carded and thermobonded non-wovens prepared from the fibres have sufficient hydrophobic properties.

The nature of the process dictates certain limits on the 25 relative amounts of wax and polydiorganosiloxane. An excessive amount of wax will increase fibre/fibre friction and in particular fibre/metal friction in the crimper, leading to increased development of heat and a risk of the filaments becoming melted together and ruined. The friction 30 conditions will also be detrimental for high speed carding. It is important that the friction-induced development of heat during carding is kept to a minimum, in particular when carding at high speeds. An excessive amount of polydiorganosiloxane will reduce friction in the crimper and 35 during carding. Fibres with an excessive of amount of

polydiorganosiloxane will be slippery and difficult to stretch and card. Such fibres are also difficult to texturize in the crimper, since this requires a certain minimum fibre/metal friction.

- 5 Similarly, considerations of hydrophobicity dictate certain limits on the relationship between the amount of antistatic agent on the one hand and the hydrophobic components (wax and polydiorganosiloxane) on the other hand.

The spin finish in the spinning section (first spin finish)  
10 should be an antistatic and lubricating finish, and should be as hydrophobic as possible.

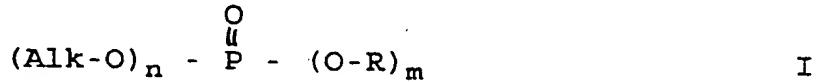
As explained above, it is known to use anionic, cationic and non-ionic antistatic agents in spin finishes. Non-ionic antistatic agents are e.g. polyethylene glycol esters and  
15 polyethylene glycol alkyl esters. These non-ionic antistatic agents are highly heat resistant and have good lubricating properties, but they do not have as efficient antistatic properties as the anionic and cationic antistatic agents. As for cationic antistatic agents, it has already been explained  
20 that these have properties which generally make them undesirable for fibres to be used for hygienic or medical purposes. In addition, amphoteric antistatic agents, i.e. agents which can function as both a cationic and anionic agent, exist, e.g. Betaine and Imidazoline.

25 Anionic antistatic agents, e.g. of the sulphate and phosphate family, are the most commonly used for the production of hygienic and medical fibres. In some cases, fatty amine and fatty acid ethoxylates are used as neutralizing agents for anionic antistatic agents in order to increase the antistatic  
30 effect without adversely affecting the friction properties of the filaments, since anionic antistatic agents are less efficient than cationic antistatic agents. However, anionic antistatic agents are more desirable for products which are designed to be in contact with the skin than are cationic

agents. A number of anionic antistatic agents in fact fulfil the FDA requirements for indirect food additives. Anionic antistatic agents are e.g. sulphated fatty acid esters, sulphated alcohols, phosphate esters of ethoxylated alcohols, 5 alkyl phosphate salts, and phosphated alcohols such as polyethylene glycol alkyl ether phosphate.

For the reasons given above, the antistatic agent is preferably an anionic or non-ionic antistatic agent, most preferably an anionic antistatic agent. The first spin finish 10 typically contains, as an antistatic agent, a phosphoric acid ester of a water-insoluble alcohol, and is typically in the form of an aqueous dispersion with an active content of about 0.5-2%. (The term "active content" in the context of the present invention refers to the non-water (non-solvent) 15 content of the spin finishes.)

A preferred antistatic agent is a neutralized phosphoric acid ester of the general formula I



20 wherein Alk is a branched or linear aliphatic alkyl or alkenyl group containing 10-24 carbon atoms; R is hydrogen, an alkali metal, an amino group, or a mono-, di- or tri-  $\beta$ -hydroxyethanol amino group; m is 0, 1 or 2 and n is 1, 2 or 3, the sum of which is 3; or a mixture of such neutralized 25 phosphoric acid esters.

Alk in the compound of formula I is in particular an alkyl group containing 12-22 carbon atoms, preferably 14-20 carbon atoms, e.g. 16-18 carbon atoms, and preferably a straight chain alkyl group. Preferred compounds are also those in 30 which n is 2 and m is 1. The ester of formula I should be solid at temperatures up to at least about 40°C, and preferably up to at least about 80°C, e.g. up to at least about 95°C.

A preferred first spin finish comprises e.g. a neutralized salt of a stearyl alcohol phosphoric acid ester and, as a lubricant and cohesion conferring agent, ethoxylated castor oil.

- 5 It is also contemplated that other types of antistatic agents may be used, e.g. sulphated fatty acid esters and phosphated alcohols such as a polyethylene glycol alkyl ether phosphate. Regardless of the specific chemical nature of the antistatic agent used in the first and second spin finishes of the  
10 present invention, it is preferably one which is permitted by FDA Vol. 21, section 177.1850 as an indirect food additive for nonwovens intended to be in contact with food.

Other suitable cohesion conferring agents are e.g. ethoxylated vegetable oils such as ethoxylated palm oil and  
15 ethoxylated coconut oil.

The active content of the first spin finish typically consists of about 80-95% by weight of the antistatic agent and about 5-20% by weight of a lubricant, more typically about 88-92% by weight of the antistatic agent and about  
20 8-12% by weight of a lubricant. The amount of the first spin finish applied to the fibres is generally in the range of about 0.08-0.25%, more typically 0.10-0.20%, by weight active content based on the weight of the fibres.

The spin finish in the stretching section (second spin  
25 finish) comprises a combination of a relatively hydrophobic antistatic agent (normally of the same type used in the first spin finish, for example a neutralized phosphoric acid alkyl ester), a hydrocarbon wax, an emulsifier and optionally a polydiorganosiloxane, normally in the form of an aqueous dispersion with an active content on the order of about 10%.

The hydrocarbon wax used in the second spin finish of the present invention is in particular a paraffin wax or microcrystalline wax. However, it is also contemplated that

natural waxes, i.e. an insect or plant wax, may also be suitable.

Paraffin wax is a crystalline hydrocarbon mixture which is solid at room temperature and which is obtained from the light petroleum fraction known as "pressable wax distillate".

Paraffin wax normally consists mainly of straight-chained hydrocarbons and some branched-chain hydrocarbons

(isoparaffins). Microcrystalline wax, which is also a hydrocarbon mixture that is solid at room temperature, is obtained from heavy petroleum distillates and residues.

Microcrystalline wax normally consists mainly of branched-chain hydrocarbons (isoparaffins) and naphthenes (large side chains) along with small amounts of straight-chain hydrocarbons and aromatic hydrocarbons.

The melting point of paraffin waxes is typically in the range of about 45-65°C, while that of microcrystalline waxes is typically in the range of about 50-95°C. (The solidifying point of a hydrocarbon wax is normally about 2-3°C below the melting point).

In the context of the present invention the term "hydrocarbon wax" refers to a paraffin or microcrystalline wax of natural or synthetic origin, in particular to a wax with a melting point in the range of 40-80°C, corresponding to an average molecular weight of about 250-800 (as determined by high

temperature gel permeation chromatography, using e.g. trichlorobenzene as an eluent, or by mass spectroscopy), or to a mixture of waxes containing a major proportion of a paraffin or microcrystalline wax and having a melting point in the above-mentioned range. While a wax or wax mixture with

a relatively low melting point (i.e. about 40-80°C) is preferred according to the present invention to ensure that the wax may be easily and uniformly distributed on the surface of the fibres without use of excessively high temperatures, it is, however, also contemplated that wax or wax mixtures having a higher melting point, e.g. up to about

120°C, will also be suitable for certain applications. Preferred hydrocarbon waxes have in particular a melting point in the range of 45-65°C, e.g. 50-60°C, corresponding to an average molecular weight in the range of about 400-600.

- 5 For waxes lying within these preferred temperature ranges, the second spin finish is typically applied at a temperature in the range of 25-60°C, e.g. 40-55°C (the fibres generally having a somewhat higher temperature during application of the second spin finish).
- 10 Since waxes normally consist of a mixture of different hydrocarbons, this will also be the case for the waxes used for the purpose of the present invention. The "wax" will therefore typically be a mixture of different wax types, some of which may be waxes having higher or lower molecular weights and melting points than those given above, as long as the melting point of the total mixture lies within the range stated above.

The wax may also contain a certain amount of a "hydrocarbon resin", i.e. a partially cross-linked hydrocarbon wax with a relatively high melting point, e.g. up to about 120°C. Hydrocarbon resins are prepared synthetically by radical polymerisation of hydrocarbon waxes containing aromatic hydrocarbons.

For wax mixtures containing other components than a hydrocarbon wax with a melting point in the range of 40-80°C, e.g. a hydrocarbon wax with a higher melting point or a hydrocarbon resin, the amount of these other components will typically comprise no more than 40% by weight of the wax mixture, preferably no more than 30% by weight of the wax mixture, more preferably no more than 20% by weight of the wax mixture.

As mentioned above, it is also contemplated that natural waxes insect or plant waxes may also be used as the wax component in the second spin finish of the present invention.

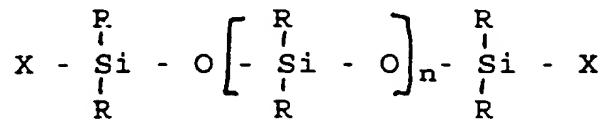
While natural waxes may contain a variety of different components, hydrocarbons are a major component in many of these. One natural wax of interest is beeswax, which contains a mixture of hydrocarbons, monoesters, diesters, triesters, 5 hydroxymonoesters, hydroxypolyesters, free acids, acid monoesters and acid polyesters, as well as a small amount of unidentified material. Other insect waxes of interest are for example those from crickets, grasshoppers and cockroaches.

The waxes of many plant species contain a major proportion of 10 hydrocarbons, mainly in the form of unbranched alkanes with an odd number of carbon atoms. However, branched alkanes as well as alkenes have also been reported and are probably present in many plant waxes. Also, some vegetable waxes, such as carnauba wax, contain a relatively small percentage of 15 unbranched alkanes. Like the animal waxes, plant waxes also contain various amounts of other components, including monoesters, diesters, hydroxyesters, polyesters, primary and secondary alcohols, acids, aldehydes, ketones, etc.

Natural waxes used for the purpose of the present invention 20 should have a melting point which lies within the ranges given above for hydrocarbon waxes.

It has been found that particularly good results in terms of improved hydrophobic properties are obtained when the second spin finish contains a polydiorganosiloxane compound 25 (silicone). Thus, in a preferred embodiment of the invention, at least 6% by weight of the active content of the second spin finish consists of the polydiorganosiloxane, typically at least 8% by weight.

The polydiorganosiloxane is in particular a 30 polydialkylsiloxane of the general formula II,



II

in which each R is independently an alkyl group containing 1-4 carbon atoms, phenyl or H, n is a number in the range of 500-3000, and X is OH, CH<sub>3</sub>, H, O-CH<sub>3</sub> or O-acetyl. A preferred polydialkylsiloxane is polydimethylsiloxane.

- 5 The content of polydiorganosiloxane in the second spin finish will obviously depend on the hydrophobic properties which are desired in the fibres. However, it is possible to define two general categories of spin finish containing polydiorganosiloxane: one for the production of fibres with a 10 medium degree of hydrophobicity, and one for the production of fibres with a very high degree of hydrophobicity. For the production of fibres having a medium hydrophobicity, the active content of the second spin finish will typically contain about 6-11% by weight of the polydiorganosiloxane, 15 e.g. about 7-10% by weight. For the production of fibres having a very high hydrophobicity, the active content of the second spin finish will typically contain at least about 12% by weight of the polydiorganosiloxane, e.g. at least about 15% by weight, more typically at least about 20% by weight, 20 and may contain as much as 35% by weight. The amount of polydiorganosiloxane in the second spin finish will in this case often be in the range of 20-30% by weight, e.g. 22-28% by weight, of the active content.

As for the antistatic agent in the second spin finish, those 25 antistatic agents discussed above in connection with the first spin finish are also suitable for the second spin finish, and the same antistatic agent may advantageously be used in both the first spin finish and the second spin finish.

- 30 The content of antistatic agent, wax and polydialkylsiloxane in the second spin finish will in each case be determined taking into consideration the carding and hydrophobic properties which are desired in the finished fibres. Thus, a certain minimum antistatic content is required in order to 35 avoid fibres which have a poor cardability due to the

- presence of a static electric charge. On the other hand, a certain maximum relative antistatic content is dictated by the need to have a certain minimum content of the hydrophobic agent (wax and polydialkylsiloxane) in order to obtain the desired degree of hydrophobicity. When very high hydrophobicity is desired, the second spin finish should include a certain amount of polydialkylsiloxane, which provides increased hydrophobicity compared to spin finishes with a wax alone as the hydrophobic agent.
- Since the hydrophobic second spin finish is an aqueous dispersion of non-water soluble components, the use of an emulsifier will normally be necessary in order to prepare and stabilize the dispersions. The precise nature of the emulsifier is not believed to be critical. Anionic emulsifiers, sulphur-containing emulsifiers, etc. are typically used, for example neutralized alkylbenzene sulphonate acid, lignin sulphonate acid and benzoic acid, since such compounds also have an advantageous corrosion-preventing effect. The emulsifier content is preferably as low as possible in order to ensure optimum hydrophobic properties in the fibres.

The active content of the second spin finish will typically comprise 10-50% by weight of the antistatic agent, 15-70% by weight of the wax, up to 35% by weight of the polydiorganosiloxane, and 5-15% by weight of the emulsifier. Preferably, the active content of the second spin finish comprises 20-45% by weight of the antistatic agent, 40-65% by weight of the wax, and about 6-28% by weight of the polydiorganosiloxane (the remainder of the active content being the emulsifier).

The second spin finish is typically applied in an amount (total active content by weight of the fibres) of about 0.25-0.60%. Together with that which is applied in the first spin finish, the finished fibres typically carry at their surface a total (by weight of the fibres) of about 0.10-0.50%

by weight of the antistatic agent, about 0.10-0.35% by weight of the hydrocarbon wax or wax mixture, from 0% to about 0.25% polydiorganosiloxane and about 0.001-0.10% of an emulsifier. More typically, the fibres carry at their surface 0.12-0.40% by weight of the antistatic agent, 0.12-0.30% by weight of the wax or wax mixture, 0.01-0.20% by weight of the polydiorganosiloxane and 0.02-0.09% by weight of the emulsifier, e.g. 0.15-0.35% by weight of the antistatic agent, 0.18-0.27% by weight of the wax or wax mixture, 10 0.03-0.15% by weight of the polydiorganosiloxane and 0.04-0.07% by weight of the emulsifier.

Fibres produced according to the present invention may also be defined according to the relative amounts, on the surface of the fibres, of the various components applied in the first 15 and second spin finishes. Thus, a particular embodiment of the invention relates to a texturized, cardable, polyolefin-based fibre carrying, at its surface, a spin finish coating comprising 25-60% by weight of an antistatic agent, 15-60% by weight of a natural or synthetic hydrocarbon wax with a 20 melting point in the range of 40-120°C or of a wax mixture comprising at least one such hydrocarbon wax and having a melting point in the range of 40-120°C, 0-30% by weight of a polydiorganosiloxane, and the remainder of an emulsifier. The spin finish coating typically comprises 30-55% by weight of 25 the antistatic agent, 25-50% by weight of the wax or wax mixture, 2-25% by weight of the polydiorganosiloxane and 4-14% by weight of the emulsifier, e.g. 35-50% by weight of the antistatic agent, 30-45% by weight of the wax or wax mixture, 6-20% by weight of the polydiorganosiloxane and 30 7-12% by weight of the emulsifier.

As mentioned above, the present invention makes it possible to "fine-tune" the hydrophobic properties as well as the fibre/fibre and fibre/metal friction properties of the fibres. Control of the hydrophobic properties is accomplished 35 by varying the ratios of the various components in the second spin finish, in particular (a) the ratio between the

antistatic agent and the hydrophobic components (wax and polydiorganosiloxane), and (b) the ratio between the wax and the polydiorganosiloxane. It has thus been found that there is a linear relationship between hydrophobicity (expressed as 5 repellency and determined as explained below based on the EDANA recommended test for nonwovens repellency (No. 120.1-80)) and the weight ratio between the amounts of antistatic agent and hydrophobic components in the second spin finish, when the repellency is plotted as a function of 10 the ratio  $A/(W+5\times S)$ , where A is the content of antistatic agent, W is the wax content, and S is the content of polydiorganosiloxane (the S content being multiplied by five).

Fig. 1 shows graphically the repellency (in cm water column) 15 of various nonwovens as a function of the above-mentioned weight ratio between the antistatic agent and the hydrophobic components ( $A/(W+5\times S)$ ). The nonwovens, which had a base weight of 22 g/m<sup>2</sup>, were prepared from polypropylene fibres using the methods described below for the Examples.

20 When the ratio  $A/(W+5\times S)$  is greater than about 1.1, the fibres are slightly hydrophobic and have an absorbency time of at least about 6 min, and the strike-through time for a 22 g/m<sup>2</sup> nonwoven produced from the fibres is about 5-10 sec. (see below regarding tests for absorbency and strike-through 25 time).

When the ratio  $A/(W+5\times S)$  is in the interval of from about 0.7 to about 1.0, the fibres have a medium degree of hydrophobicity and have an absorbency time of more than about 20 min, and the strike-through time for a 22 g/m<sup>2</sup> nonwoven 30 produced from the fibres is greater than 10 sec.

When the ratio  $A/(W+5\times S)$  is less than about 0.7, the fibres are highly hydrophobic and have an absorbency time of more than about 24 hours, and the strike-through time for a 22 g/m<sup>2</sup> nonwoven produced from the fibres is more than 120 sec.

The hydrophobic properties of the fibres can also be expressed in terms of the contact angle between water and the surface of the fibres. Fibres with non-wettable  
5 characteristics should have a contact angle of more than 90° (as measured e.g. using the Wilhelmy technique-force measurement for single fibre wettability). It is believed that the slightly hydrophobic fibres of the present invention will have a contact angle of slightly above 90°, while the  
10 highly hydrophobic fibres will have a contact angle that approaches 180° (a contact angle of 180° being a theoretical maximum for total non-wetting).

Control of the fibres' processing characteristics, i.e. fibre/fibre and fibre/metal friction, is obtained by varying  
15 the relationship between the wax and the polydiorganosiloxane in the second spin finish. It has thus been found that the weight ratio S/W (where S is polydiorganosiloxane and W is wax) can vary from about 0.1 to about 2 (assuming of course that polydiorganosiloxane is present in the second spin  
20 finish), and that a significant change in the properties of the fibres occurs at a ratio of about 1, so that a S/W weight ratio of less than 1 gives fibres with a high fibre/fibre and fibre/metal friction and a moderate to high hydrofobicity, while a S/W weight ratio of more than 1 gives more slippery  
25 fibres which are highly hydrophobic but which have a relatively low fibre/fibre and fibre/metal friction. Fibres without any polydiorganosiloxane will have a high fibre/fibre and fibre/metal friction and a moderate hydrophobicity.

As mentioned above, one of the major advantages of the fibres  
30 of the present invention is that they are suitable for high-speed carding, this being of particular interest for polypropylene fibres. Thus, the fibres of the present invention may be processed to a uniform carding web at high speeds in the carding machine, typically at least about 80  
35 m/min, such as at least 100 m/min, and (in particular for polypropylene fibres) in many cases at least 150 m/min or

even 200 m/min or more. The carding speed chosen in each case will depend on factors such as the type of fibre (e.g. polypropylene, polyethylene, bicomponent, etc.) and the nature of the nonwoven being produced. Carding will typically 5 be by means of a dry-laid carding process.

Polypropylene fibres according to the invention are preferably able to be carded, at a carding speed of at least 100 m/min, preferably at least 150 m/min, more preferably at least 200 m/min, into a web which can be thermally bonded to 10 a nonwoven in which the ratio between the tensile strength in the machine direction and the tensile strength in the cross direction is at the most 7, preferably at the most 5 (the strengths being determined as explained below). Polypropylene/polyethylene bicomponent fibres of the present 15 invention are preferably able to be carded, at a carding speed of at least 80 m/min, preferably at least 100 m/min, into a web which can be thermally bonded to a nonwoven in which the ratio between the tensile strength in the machine direction and the tensile strength in the cross direction is 20 at the most 6. Polyethylene fibres of the present invention are preferably able to be carded, at a carding speed of at least 80 m/min, into a web which can be thermally bonded to a nonwoven in which the ratio between the tensile strength in the machine direction and the tensile strength in the cross 25 direction is at the most 5. In all cases, the randomization of fibres in the web expressed as the ratio between the two tensile strengths should be as close to 1 as possible.

The strengths of different nonwoven materials may be compared by using a so-called "bondability index", which compensates 30 for differences in fibre randomization and which is calculated as explained below on the basis of nonwoven tensile strength measured in the machine direction and the cross direction. A standardized carding test for determining the tensile strength of nonwovens is performed as follows:

From about 95-105 kg of fibres, webs of at least 15 kg with a base weight of 20-25 g/m<sup>2</sup> fibre web are produced by carding at the chosen speed at optimum roller settings with respect to evenness of the web. The webs are subsequently

5 thermobonded, the individual webs being thermobonded at different temperatures at intervals of typically 2°C within a range chosen according to the type of fibres. For polypropylene fibres, a web with a base weight of about 20 g/m<sup>2</sup> is prepared by thermobonding at temperatures in the

10 range of 145-157°C, using a calender pressure of 64 N/mm and a typical carding speed of 100 m/min. For polyethylene fibres, a web with a base weight of about 25 g/m<sup>2</sup> is prepared by thermobonding at temperatures in the range of 126-132°C, with a calender pressure of 40 N/mm and a typical carding

15 speed of 80 m/min. For bicomponent fibres with a polypropylene core and a polyethylene sheath, a web with a base weight of about 20 g/m<sup>2</sup> is prepared by thermobonding at temperatures in the range of 137-147°C, with a calender pressure of 40 N/mm and a typical carding speed of 80 m/min.

20 The tensile strengths of the webs are then determined in the machine direction and the cross direction, the measurements being performed according to the EDANA recommended test: Nonwovens Tensile Strength, 20 February, 1989, which is based on ISO 9073-3:1989 ("Determination of tensile strength and

25 elongation"); however, for the purposes of the present invention the relative humidity was between 50% and 65%. Finally, a bondability index is calculated for each of the bonding temperatures, the bondability index being defined as the square root of the product of the machine direction

30 strength and the cross direction strength. In order to arrive at a standard bondability index for a standard nonwoven base weight of 20 g/m<sup>2</sup> (BI<sub>20</sub>), the calculated bondability index for a given sample is multiplied by 20 and divided by the actual base weight in g/m<sup>2</sup>, thereby compensating for the fact

35 that the strength of a nonwoven varies with the base weight.

For polypropylene-based fibres, the bondability index (BI<sub>20</sub>) should be at least 15 N/5 cm when carded at a speed of 100

m/min and at least 10 N/5 cm when carded at a speed of 150 m/min, and is preferably at least 17 N/5 cm when carded at a speed of 100 m/min and at least 10 N/5 cm when carded at a speed of 150 m/min.

- 5 For polyethylene-based fibres, the bondability index ( $BI_{20}$ ) should be at least 7 N/5 cm when carded at a speed of 80 m/min, and is preferably at least 10 N/5 cm when carded at a speed of 80 m/min.

For sheath-and-core type bicomponent fibres having a  
10 polypropylene-based core and a polyethylene-based sheath, the bondability index ( $BI_{20}$ ) should be at least 8 N/5 cm when carded at a speed of 80 m/min, and is preferably at least 10 N/5 cm at 80 m/min.

15 The hydrophobic properties of nonwovens prepared from the fibres of the invention may be tested according to various methods. These include a repellency test, a test for liquid absorbency time, a test for liquid strike-through time and a runoff test. The test for liquid absorbency time may also be used for testing the hydrophobic properties of fibres.

- 20 The repellency test is performed according to the EDANA recommended test for nonwovens repellency (No. 120.1-80), with conditioning of the samples for at least 2 hours at a temperature of 23°C and a relative humidity of 50%. This test involves measuring the pressure (expressed as cm water column) required to effect water penetration through a nonwoven subjected to an increasing water pressure. Briefly, a circular section of a nonwoven sample of the desired base weight (typically about 22 g/m<sup>2</sup>) with a diameter of 60 mm is subjected to a water column whose height increases at a rate 25 of 3 cm/min., and the repellency of the nonwoven is determined as the height of the water column at the moment 30 when the third drop of water penetrates the sample.

In the above repellency test, nonwovens containing the fibres of present invention should show a repellency of at least about 1.5 cm. For nonwovens prepared from fibres with a medium degree of hydrophobicity, the repellency should be at 5 least about 2.5 cm, typically at least about 3 cm. For nonwovens containing highly hydrophobic fibres the repellency should be at least about 4 cm, more preferably at least about 5 cm, e.g. at least about 6 cm.

Another suitable test method for determining the hydrophobic 10 properties of nonwovens is a test for liquid absorbency time according to the EDANA recommended test for nonwovens absorption (No. 10.1-72). This test involves determining the time required for the complete wetting of a specimen strip (5 g) loosely rolled into a cylindrical wire basket (3 g) and 15 dropped onto the surface of the liquid (typically water) from a height of 25 mm. Nonwoven samples for use in this test are for the purpose of the present invention conditioned for at least 2 hours at a temperature of 23°C and a relative humidity of 50%.

20 The above liquid absorbency test may also be used, with certain minor amendments, for determining the hydrophobic properties of fibres. In this case, the EDANA test procedure for nonwovens is amended by conditioning the fibre samples at a temperature of 45°C and at a relative humidity of less than 25 10% for one hour prior to testing, the samples being allowed to cool to 23°C before testing. For determining the absorbency of fibres, a carding web with a base weight of approximately 10 g/m<sup>2</sup> is prepared from the fibres to be tested by carding at 15 m/min., and samples having a weight 30 of 5 g are then taken from the web. The remainder of the test is carried out according to the EDANA test procedure (10.1-72). When testing either nonwovens or fibres, the absorbency time is defined as the time interval from the moment the wire basket containing the nonwoven or fibre sample hits the 35 liquid to the moment the sample is completely immersed under the surface of the liquid.

In the above test for liquid absorbency in water, the wetting time (i.e. the sinking time) for a sample of hydrophobic fibres should be at least about 6 minutes, preferably at least about 10 minutes, more preferably at least about 20 minutes, e.g. at least about 1 hour. For highly hydrophobic fibres the wetting time should be at least about 24 hours.

A further test for determining the hydrophobic properties of nonwovens is a test for liquid strike-through time (EDANA recommended test: Nonwoven coverstock liquid strike-through time (simulated urine); No. 150.1-90). In this test, the time required for a known volume of liquid to pass through a nonwoven is measured. The liquid is applied to the surface of a test piece of nonwoven coverstock which is in contact with an underlying standard absorbent pad. The test is designed to compare the strike-through time of different nonwoven coverstocks.

The nonwoven samples are for the purpose of the present invention conditioned for at least 2 hours at a temperature of 23°C and a relative humidity of 50%. 5 ml of the test liquid (a 0.9% aqueous NaCl solution) is discharged onto the sample (typical base weight 22 g/m<sup>2</sup>) in 3.75 sec., and the time required for the liquid to penetrate the nonwoven is measured electronically.

In the liquid strike-through test, nonwovens according to the present invention should have a strike-through time of at least about 5 sec., preferably at least about 10 sec., more preferably at least 15 sec. For nonwovens containing highly hydrophobic fibres the strike-through time should be at least 1 min., preferably at least about 2 min., and more preferably at least about 5 min.

The hydrophobicity of nonwovens may further be determined by evaluating the runoff percentage according to the following procedure:

Runoff is measured using simulated urine (68-72 dyne/cm; 19.4 g urea, 8 g NaCl, 0.54 g MgSO<sub>4</sub> (anhydrous), 1.18 g CaCl<sub>2</sub>·6H<sub>2</sub>O, 970.9 g demineralised water). The test involves pouring 25 ml of test liquid onto a test material (31 cm in 5 the machine direction and 14 cm in the cross direction) containing a top layer of a nonwoven coverstock and a bottom layer of filter paper, the test material being placed at angle of 10 degrees from horizontal and a collecting tray being placed under the lower end of the test material. The 10 coverstock should be placed in the machine direction with the embossed side upwards. The runoff percentage is defined as the amount of test liquid which is collected in the tray, expressed as a percentage of the original 25 ml of liquid. A good hydrophobic nonwoven should using this method give a 15 runoff of at least 90%, preferably at least 95%. For materials with superior hydrophobic properties, the runoff percentage is preferably at least 98%, and can be as high as 99% or more (which essentially corresponds to 0% penetration). In addition to the hydropobicity of the fibres 20 used to prepare the nonwoven, the runoff percentage is also to a certain extent dependent upon the weight of the material, a heavier material giving a slightly higher runoff percentage, the above-mentioned runoff percentages being based on nonwovens with a base weight of 20 g/m<sup>2</sup>.

## EXAMPLES

Fibres and nonwovens were prepared as follows:

The polyolefin raw material (polypropylene, polyethylene, or, for bicomponent fibres, polypropylene for the core and

5 polyethylene for the sheath) was spun into fibres by conventional spinning (long spinning) technology, using spinning speeds of 1500-2000 m/min for polypropylene fibres, 800-1000 m/min for PP/PE bicomponent fibres, and 300-500 m/min for polyethylene fibres, resulting in a bundle of  
10 several hundred filaments. For blue polypropylene fibres, 0.1% of phthalocyanine blue pigment was added to the raw material prior to spinning. After quenching of the filaments by air cooling, the filaments were treated with a first spin finish containing, as an antistatic agent, a neutralized  
15 C<sub>16</sub>-C<sub>18</sub> alcohol phosphoric acid ester of which the major part was a neutralized stearyl alcohol phosphoric acid ester (Silastol F203, from Schill & Seilacher, Germany) and an ethoxylated castor oil (Silastol 360, from Schill & Seilacher, Germany) by means of a lick roller. The amounts  
20 (active content) of the two compounds applied at this stage varied somewhat, but generally about 0.12-0.20% by weight of the C<sub>16</sub>-C<sub>18</sub> alcohol phosphate ester and about 0.010-0.020% by weight of the ethoxylated castor oil was applied (these amounts being by weight of the filaments).

25 The filaments were off-line stretched in a two-stage drawing operation using a combination of hot rollers and a hot air oven, with temperatures in the range of 115-135°C for polypropylene fibres, 110-120°C for PP/PE bicomponent fibres, and 95-105°C for polyethylene fibres. The stretch ratios

30 varied between 1.05:1 and 4.5:1, depending on the type of fibre (generally from 1.05:1 to 1.5:1 for polypropylene fibres and about 4:1 for polyethylene fibres and bicomponent fibres). The stretched filaments were then treated (by means of a lick roller) with different second spin finishes. The  
35 second spin finishes were aqueous dispersions containing

varying amounts of antistatic agent (the C<sub>16</sub>-C<sub>18</sub> alcohol phosphate ester mentioned above), wax and polydimethylsiloxane (silicone). The dispersions were prepared primarily by mixing the proprietary mixtures

- 5 Silastol F203, Silastol 5072 and Silastol E172 (all from Schill & Seilacher, Germany) in various ratios. The wax component was a hydrocarbon wax mixture, about 80% of which was a hydrocarbon wax with a melting point of about 55°C (average molecular weight about 500) and about 20% of which  
10 was a hydrocarbon resin with a melting point of about 120°C (average molecular weight about 1300).

The filaments were then crimped in a stuffer-box crimper and subsequently annealed in an oven at a temperature of about 125°C for polypropylene fibres, 105°C for PP/PE bicomponent  
15 fibres and 95°C for polyethylene fibres to reduce contraction of the fibres during the thermal bonding process and to allow the hydrophobic components of the second spin finish (i.e. wax and silicone) to become uniformly distributed on the surface of the filaments. Staple fibres were then produced by  
20 cutting the filaments to the desired length.

The fineness of the finished fibres was measured according to DIN 53812/2, the elongation at break and tenacity of the fibres was measured according to DIN 53816, and the crimp frequency was measured according to ASTM D 3937-82.

- 25 Nonwovens were prepared from the various fibres by carding at various speeds and thermally bonding the webs at various temperatures (see Table 2). For each nonwoven, the tensile strength and elongation was measured in both the machine direction and the cross direction as described above (i.e.  
30 using the EDANA recommended test), and a bondability index was calculated as described above on the basis of the measured tensile strengths. For comparison purposes, the bondability indices were as explained above converted to an index for a standard nonwoven with a base weight of 20 g/m<sup>2</sup>  
35 (BI<sub>20</sub>). In addition, the runoff percentage, strike-through

and repellency were also determined, the methods used also being those described above.

In the tables below, the fibre properties of a number of different fibres prepared as described above are given, along 5 with the properties of nonwovens prepared from these fibres.

Table 1 shows, in addition to the type of fibre, the following characteristics of the fibres: fineness (dtex), tenacity (cN/dtex), elongation at break (%), length (mm), crimps per 10 cm, total amount of spin finish applied (i.e.

10 the total active content applied as first and second spin finish, in percent by weight of the fibres), the composition of the total spin finish applied (percent by weight antistatic agent, wax, silicone and emulsifier), and the liquid absorbency time of the fibres.

15 Table 2 shows the following characteristics of nonwovens prepared from the fibres of Table 1: carding speed (m/min), bonding temperature (°C), maximum tensile strength in the machine direction (MD-max; N/5 cm), elongation at break in the machine direction (MD-max; %), maximum tensile strength 20 in the cross direction (CD-max; N/5 cm), elongation at break in the cross direction (CD-max; %), maximum bondability index (BI-max), standard bondability index (BI<sub>20</sub>), base weight (g/m<sup>2</sup>), runoff percentage, repellency (cm), strike-through and a rough classification of the cardability.

25 The cardability, i.e. the suitability of the fibres for carding was determined using a simple web cohesion test. This test is carried out by measuring the length a thin carding web of approximately 10 g/m<sup>2</sup> can support in a substantially horizontal position before it breaks due to its own weight, 30 the length of the carding web being increased at a rate of about 15 m/min. This is performed by taking the carding web off the card in a horizontal direction at a speed of 15 m/min, which is the carding speed used for this test.

A higher cardability as a result of a higher fibre/fibre friction gives a higher web cohesion length. The fibre/fibre friction is dependent upon factors such as the composition of the second spin finish and the degree of texturization, as well as how permanent the texturization is. Fibre/metal friction is also important for the cardability; if it is either too high or too low, the fibres are difficult to transport through the card.

Fibres which are well suited for carding will typically be able to support about 1.0 m or more in the above-described web cohesion length test. Polypropylene fibres will typically be able to support somewhat more, e.g. about 1.5-2.25 m.

TABLE 1. FIBRE DATA

Nr.	Type	Fine-ness dtex	Tenacity cN/dtex	Elong. at break %	Length mm	Crimps per 10 cm	Total spin finish %	Anti- static agent %	Wax %	Silicone %	Emulsi- fier %	Liquid abbor- bency time
1*	PP	2.36	1.67	366	40	110	0.68	39 <sup>a</sup>	37	0	0	< 1 min
2	PP	2.34	1.85	411	40	105	0.65	51.5	40.1	0	8.4	6-10 min
3	PP	2.3	1.89	403	40	96	0.65	49.29	37.3	4.64	8.76	20-120 min
4	PP	2.23	1.87	411	40	92	0.66	41.86	39.98	8.15	10.02	20-120 min
5	PP	2.28	1.89	419	40	86	0.46	44.54	33.97	10.68	10.8	> 24h
6	PP	2.28	1.89	419	40	86	0.65	36.56	39.91	12.55	10.98	> 24h
7	PP	2.24	1.82	361	43	89	0.67	34.27	37.66	16.66	11.41	> 24h
8	PP	2.32	1.87	428	42	89	0.58	57.49	15.11	19.23	8.17	> 24h
9*	PP	2.27	1.83	400	39	89	0.60	65.55	0	27.28	7.17	> 24h
10	PP	2.30	1.85	398	42	97	0.65	52	40	0	8	6-10 min
11	PP	2.29	1.86	415	42	100	0.65	49	37	5	9	20-120 min
12	PP	2.38	1.86	382	41	76	0.63	34	38	17	1.1	> 24h
13	PP-B	2.23	2.09	334	40	105	0.63	49.12	37.22	4.63	9.03	20-120 min
14	PP-B	2.23	2.09	334	40	105	0.66	50.22	34.41	6.12	9.25	20-120 min
15	PP-B	2.18	2.07	329	48	102	0.63	34.28	37.66	16.66	11.41	> 24h
16	ES-E	3.28	3.1	135	41	87	0.63	50.39	36.14	4.66	8.8	20-120 min
17*	ES-E	3.27	3.06	125	42	89	0.47	37.08	0	53.67	9.25	> 24h
18	ES-C	2.2	3.3	126	40	85	0.67	51.01	32.54	7.37	9.08	> 24h
19	PE	3.2	2.15	213	48	94	0.58	49.57	37.17	4.63	8.63	20-120 min
20	PE	3.2	2.15	213	48	94	0.55	47.23	32.71	12.14	7.91	> 24h
21	PE	3.39	2.07	237	45	105	0.55	45.34	29.8	16.62	8.25	> 24h
22*	PE	3.2	2.15	213	48	94	0.41	29.27	0	57.63	13.09	> 24h

<sup>a</sup>+24% hydrophilic antistatic agent from 1st spin finish

PP: polypropylene

PP-B: blue polypropylene

ES-E: eccentric bicomponent (polypropylene core/polyethylene sheath)

ES-C: concentric bicomponent (polypropylene core/polyethylene sheath)

PE: polyethylene

\* comparative example

TABLE 2. NONWOVEN PROPERTIES (fibres of Table 1)

Nr.	Line Speed m/min	Bonding temp. °C	Strength MD-max N/5cm	Elong. MD-max %	Strength CD-max N/5cm	Elong. CD-max %	BI-max N/5cm	BI <sub>20</sub> N/5cm	Base Weight g/m <sup>2</sup>	Runoff %	Repel- lency cm water col.	Strike through Sec.	Carda- bility
1*	100	149	36.4	50.4	7.4	104.8	19.0	20.3	1	-	-	good	
2	100	149	38.1	61.8	8.3	101	18	20.9	94.0	1.5	7.5	good	
3	100	155	36.5	69	11.1	105.6	20.41	18.6	21.7	100	3.2	12.0	good
4	100	153	36.6	79.6	10.8	101.8	19.23	17.5	21.4	99.5	4.0	15	good
5	100	153	40	72.4	11.1	119.5	20.18	18.3	21.6	99.0	5.0	18	good
6	100	151	35.8	63.4	9.9	90.7	18.8	17.1	22.2	98.5	4.0	10.5	good
7	100	153	35.7	68.2	11.7	93.6	19.11	17.4	22.4	100	6.5	>300	good
8	100	153	39.7	42.2	10.7	96.1	21.7	19.7	20.9	100	5.3	>120	fair <sup>1</sup>
9*	100	155	25.3	25.7	5.3	64.3	11.58	10.5	23	98	5.5	40	fair <sup>1</sup>
10	150	149	36.2	65.4	6.4	90.8	15.2	13.5	22.6	97.0	1.6	5.9	good
11	150	151	33.6	43.0	5.1	68.0	13.1	12.2	21.4	100	3.5	18.5	good
12	151	154	24.6	28.5	5.7	80.9	11.8	10.8	22.0	100	6.5	41	good
13	100	155	48.4	51.8	10.9	95.9	19.46	17.7	23.4	98.5	4.0	15	good
14	100	153	37.2	41.6	9.5	78.8	15.59	14.2	23	91.0	-	106	good
15	100	147	27.2	47.4	8.8	73.4	13.9	12.9	21.5	99.0	3.5	29	good
16	80	139	12.2	11.5	2.9	69.7	7	20.8	93	-	-	20	good
17*	80	147	18.7	10.9	3.4	61.4		8	20.7	97.5	4.2	15	poor
18	80	147	37.3	15.5	5.7	64.9		13.8	20.7	96.0	-	16	good
19	80	130	32.2	26.7	6	82.1	13.6	11.5	25.6	96.5	-	58	good <sup>2</sup>
20	80	126	26	36.9	8.5	95.6	13	9.2	28.2	94.5	-	156	Fair <sup>3</sup>
21	80	126	33.2	34.6	7	80.8	13.5	9.9	27.4	95.5	-	13	Fair <sup>3</sup>
22*	51	126	35.5	33	7	59.5	17.6	11.5	30.7	95.5	-	158	poor

\* Comparative example

<sup>1</sup> slippery fibre<sup>2</sup> uneven nonwoven<sup>3</sup> unstable carding

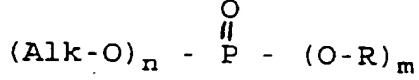
A number of things can be deduced from Tables 1 and 2, including the fact that an increased amount of silicone on the fibres (from the second spin finish) results in fibres and nonwovens with increased hydrophobicity, and that the 5 ratio between the antistatic agent and the hydrophobic components (wax and silicone) also is important for the hydrophobicity. Furthermore, a number of things become apparent from the comparative examples in Tables 1 and 2 (i.e. Examples 1, 9, 17 and 22). Thus, Example 1 shows the 10 significance of the hydrophobic nature of the antistatic agent in the first spin finish. In this case, the antistatic agent in the first spin finish was hydrophilic (a neutralized phosphate ester of n-butanol), and as a result, the fibres and resulting nonwovens were also hydrophilic despite the 15 presence of wax and a hydrophobic antistatic agent in the second spin finish. Example 9 shows fibres which contain only silicone as the hydrophobic component. These fibres are highly hydrophobic, but are also very slippery and have relatively poor carding properties, with nonwovens prepared 20 from these fibres having a low bondability index compared to polypropylene fibres prepared according to the invention. Example 17 shows another type of fibre treated with only silicone as the hydrophobic component. In this case, the antistatic agent was applied only in the first spin finish, 25 and the low ratio between the antistatic agent and the silicone resulted in fibres with a high degree of static electricity and therefore poor cardability. Example 22 is similar to Example 17, although with polyethylene fibres.

In tests carried out in connection with the present 30 invention, it has been found that there is a good correlation between the results for absorbency time (expressed in minutes) and the results for water repellency (expressed in cm water column), a fair mathematical correlation being:

$$\ln(\text{abs. time (min.)}) = -0.98 + 1.6 \text{ (cm water col.)}$$

## CLAIMS

1. A method for producing cardable, hydrophobic polyolefin-based staple fibres, the method comprising the following steps:
  - 5 a. applying to spun filaments a first spin finish comprising an antistatic agent,
  - b. stretching the filaments,
  - c. applying to the stretched filaments a second spin finish in the form of a dispersion comprising i) an antistatic agent, ii) a natural or synthetic hydrocarbon wax with a melting point in the range of 40-120°C, or a wax mixture comprising at least one such hydrocarbon wax and having a melting point in the range of 40-120°C, and optionally iii) a polydiorganosiloxane,
  - 10 d. crimping the filaments,
  - e. drying the filaments, and
  - f. cutting the filaments to obtain staple fibres.
2. A method according to claim 1, wherein the fibres are produced by conventional spinning (long spinning) technology.
- 20 3. A method according to claim 1 or 2 wherein the antistatic agent is an anionic or non-ionic antistatic agent.
4. A method according to any of claims 1-3 wherein the antistatic agent in the first spin finish is the same as the antistatic agent in the second spin finish.
- 25 5. A method according to any of claims 1-4 wherein the antistatic agent is a neutralized phosphoric acid ester of the general formula I



I

- 30 wherein Alk is a branched or linear aliphatic alkyl or alkenyl group containing 10-24 carbon atoms; R is hydrogen, an alkali metal, an amino group, or a mono-, di- or tri-  $\beta$ -

hydroxyethanol amino group; m is 0, 1 or 2 and n is 1, 2 or 3, the sum of which is 3; or a mixture of such neutralized phosphoric acid esters.

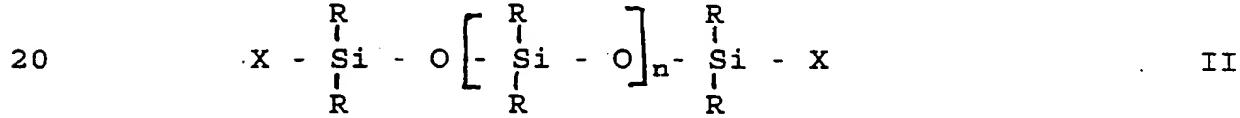
6. A method according to claim 5 wherein Alk in the compound  
5 of formula I is an alkyl group containing 12-22 carbon atoms, preferably 14-20 carbon atoms, in particular 16-18 carbon atoms.

7. A method according to claim 6 wherein Alk in the neutralized phosphoric acid ester of the general formula I is  
10 a straight chain alkyl group.

8. A method according to any of claims 5-7 wherein n is 2 and m is 1.

9. A method according to any of claims 1-8 wherein the hydrocarbon wax or wax mixture has a melting point in the  
15 range of 40-80°C, preferably 45-65°C, e.g. 50-60°C.

10. A method according to any of claims 1-9 wherein the second spin finish comprises a polydialkylsiloxane of the general formula II,



in which each R is independently an alkyl group containing 1-4 carbon atoms, phenyl or H, n is a number in the range of 500-3000, and X is OH, CH<sub>3</sub>, H, O-CH<sub>3</sub> or O-acetyl.

25 11. A method according to claim 10 wherein the polydialkylsiloxane is polydimethylsiloxane.

12. A method according to any of claims 1-11 wherein the active content of the second spin finish comprises 10-50% by weight of the antistatic agent, 15-70% by weight of the wax,

up to 35% by weight of the polydiorganosiloxane, and 5-15% by weight of an emulsifier.

13. A method according to claim 12 wherein at least 6% by weight of the active content of the second spin finish

5 consists of the polydiorganosiloxane.

14. A method according to claim 13 wherein the active content of the second spin finish comprises 20-45% by weight of the antistatic agent, 40-65% by weight of the wax and 6-28% by weight of the polydiorganosiloxane.

10 15. A texturized, cardable, polyolefin-based fibre carrying, at its surface, 0.10-0.50% by weight of the fibre of an antistatic agent, 0.10-0.35% by weight of the fibre of a natural or synthetic hydrocarbon wax with a melting point in the range of 40-120°C or of a wax mixture comprising at least 15 one such hydrocarbon wax and having a melting point in the range of 40-120°C, 0-0.25% by weight of the fibre of a polydialkylsiloxane, and 0.001-0.10% by weight of the fibre of an emulsifier.

16. A fibre according to claim 15 which carries at its

20 surface 0.12-0.40% by weight of the antistatic agent, 0.12-0.30% by weight of the wax or wax mixture, 0.01-0.20% by weight of the polydiorganosiloxane and 0.02-0.09% by weight of the emulsifier.

17. A fibre according to claim 16 which carries at its

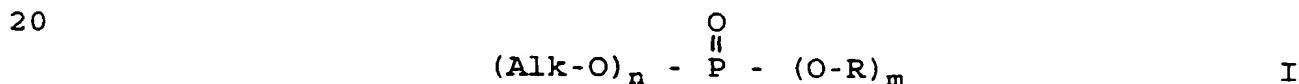
25 surface 0.15-0.35% by weight of the antistatic agent, 0.18-0.27% by weight of the wax or wax mixture, 0.03-0.15% by weight of the polydiorganosiloxane and 0.04-0.07% by weight of the emulsifier.

18. A texturized, cardable, polyolefin-based fibre carrying,

30 at its surface, a spin finish coating comprising 25-60% by weight of an antistatic agent, 15-60% by weight of a natural or synthetic hydrocarbon wax with a melting point in the

range of 40-120°C or of a wax mixture comprising at least one such hydrocarbon wax and having a melting point in the range of 40-120°C, 0-30% by weight of a polydiorganosiloxane, and the remainder of an emulsifier.

- 5 19. A fibre according to claim 18 wherein the spin finish coating comprises 30-55% by weight of the antistatic agent, 25-50% by weight of the wax or wax mixture, 2-25% by weight of the polydiorganosiloxane and 4-14% by weight of the emulsifier.
- 10 20. A fibre according to claim 19 wherein the spin finish coating comprises 35-50% by weight of the antistatic agent, 30-45% by weight of the wax or wax mixture, 6-20% by weight of the polydiorganosiloxane and 7-12% by weight of the emulsifier.
- 15 21. A fibre according to any of claims 15-20 wherein the antistatic agent is an anionic or non-ionic antistatic agent.
- 22. A fibre according to claim 21 wherein the antistatic agent is a neutralized phosphoric acid ester of the general formula I



wherein Alk is a branched or linear aliphatic alkyl or alkenyl group containing 10-24 carbon atoms; R is hydrogen, an alkali metal, an amino group, or a mono-, di- or tri-  $\beta$ -hydroxyethanol amino group; m is 0, 1 or 2 and n is 1, 2 or 3, the sum of which is 3; or a mixture of such neutralized phosphoric acid esters.

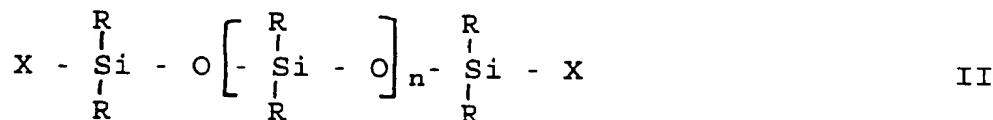
- 23. A fibre according to claim 22 wherein Alk in the compound of formula I is an alkyl group containing 12-22 carbon atoms, preferably 14-20 carbon atoms, in particular 16-18 carbon atoms.

24. A fibre according to claim 23 wherein Alk in the neutralized phosphoric acid ester of the general formula I is a straight chain alkyl group.

25. A fibre according to any of claims 22-24 wherein n is 2  
5 and m is 1.

26. A fibre according to any of claims 15-25 wherein the hydrocarbon wax or wax mixture has a melting point in the range of 40-80°C, preferably 45-65°C, e.g. 50-60°C.

27. A fibre according to any of claims 15-26 wherein the  
10 second spin finish comprises a polydialkylsiloxane of the general formula II,



15 in which each R is independently an alkyl group containing 1-4 carbon atoms, phenyl or H, n is a number in the range of 500-3000, and X is OH, CH<sub>3</sub>, H, O-CH<sub>3</sub> or O-acetyl.

28. A fibre according to claim 27 wherein the polydialkylsiloxane is polydimethylsiloxane.

20 29. A fibre according to any of claims 15-28 which is a polypropylene fibre that is able to be carded, at a carding speed of at least 100 m/min, preferably at least 150 m/min, more preferably at least 200 m/min, into a web which can be thermally bonded to a nonwoven in which the ratio between the  
25 tensile strength in the machine direction and the tensile strength in the cross direction is at the most 7, preferably at the most 5.

30 30. A fibre according to any of claims 15-29 which shows a liquid absorbency time of at least about 6 minutes, preferably at least about 10 minutes, more preferably at

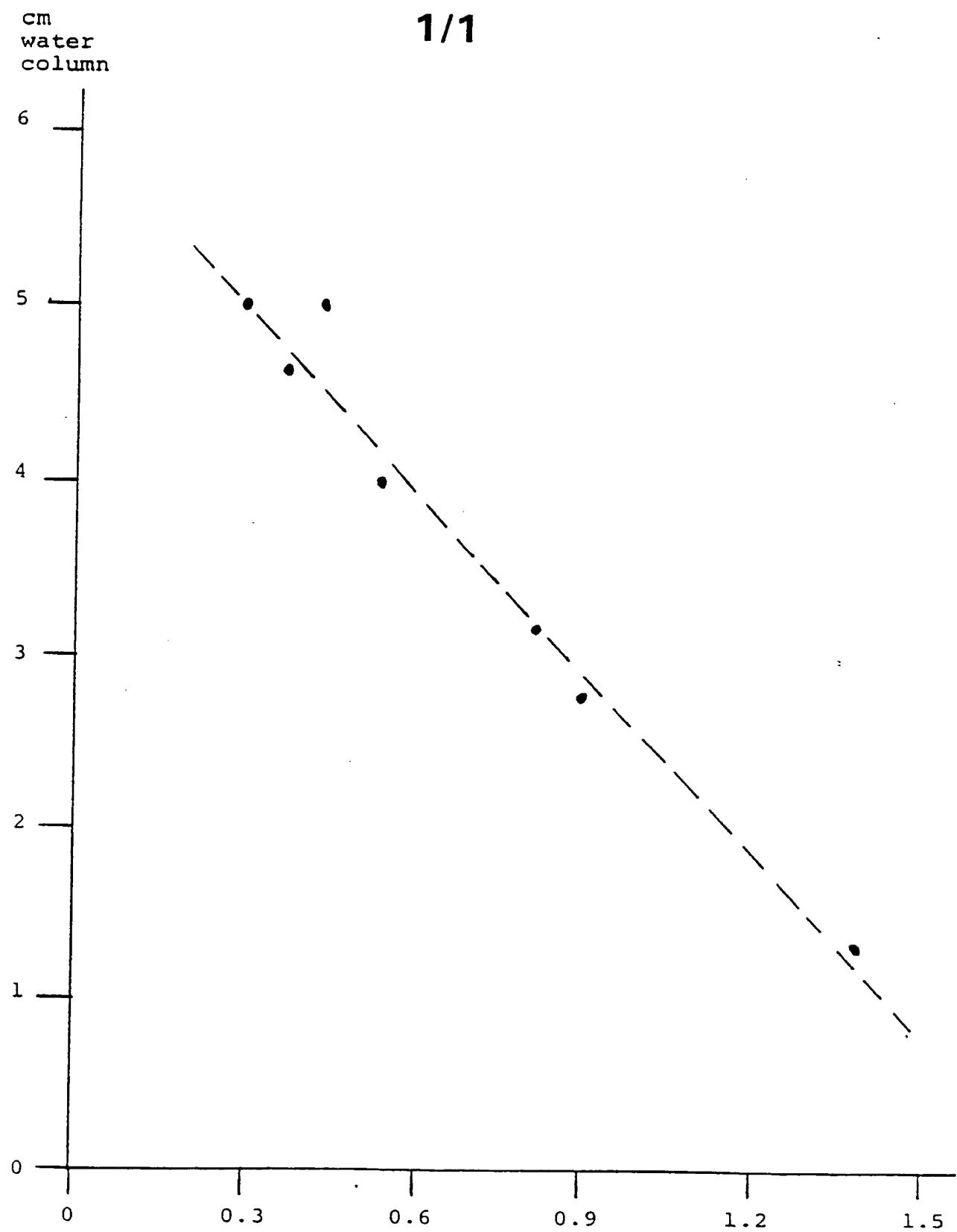
least about 20 minutes, more preferably at least about 1 hour, most preferably at least about 24 hours, as determined according to the EDANA recommended test for nonwovens absorption (No. 10.1-72) on samples taken from a carding web with a base weight of approximately 10 g/m<sup>2</sup> prepared by carding at 15 m/min, the samples having been conditioned at a temperature of 45°C and at a relative humidity of less than 10% for one hour prior to testing and allowed to cool to 23°C before testing.

10 31. A hydrophobic nonwoven material comprising the fibres according to any of claims 15-30.

32. A nonwoven material according to claim 31 which has a runoff percentage of at least 90%, preferably at least 95%, e.g. at least 98%, as determined by pouring 25 ml of simulated urine onto a test material (31 cm in the machine direction and 14 cm in the cross direction) containing a top layer of a nonwoven coverstock with a base weight of 20 g/m<sup>2</sup> and a bottom layer of filter paper, the test material being placed at angle of 10 degrees from horizontal and a collecting tray being placed under the lower end of the test material, the coverstock being placed in the machine direction with the embossed side upwards, the runoff percentage being the amount of test liquid which is collected in the tray expressed as a percentage of the original 25 ml of liquid.

33. A nonwoven material according to claim 31 or 32 which shows a repellency of at least 1.5 cm, preferably at least 2.5 cm, more preferably at least 4 cm, most preferably at least 6 cm, as determined according to the EDANA recommended test for nonwovens repellency (No. 120.1-80), the nonwoven samples having been conditioned for at least 2 hours at a temperature of 23°C and a relative humidity of 50% prior to testing.

34. A nonwoven material according to any of claims 31-33 which has a strike-through time of at least about 5 sec., typically at least about 10 sec., preferably at least 15 sec., more preferably at least 1 min., most preferably at 5 least about 2 min., as determined by the EDANA recommended test for nonwoven coverstock liquid strike-through time (No. 150.1-90), the nonwoven samples having been conditioned for at least 2 hours at a temperature of 23°C and a relative humidity of 50% prior to testing.
- 10 35. A method for preparing a hydrophobic nonwoven material, comprising processing fibres according to any of claims 15-30 to obtain a web for bonding, and thermobonding the resulting web to obtain the hydrophobic nonwoven material.



**Fig. 1**

A  
W + 5S

## INTERNATIONAL SEARCH REPORT

Int. Application No.

PCT/DK 94/00091

A. CLASSIFICATION OF SUBJECT MATTER  
 IPC 5 D06M13/292 D06M15/227

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
 IPC 5 D06M C10M D01F

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP,A,0 486 158 (HERCULES) 20 May 1992 see claims; example 1 ---	1
A	DE,A,33 34 575 (SANDOZ) 5 April 1984 see claims ---	1
A	FR,A,2 351 152 (DU PONT) 9 December 1977 see claims -----	1

 Further documents are listed in the continuation of box C. Patent family members are listed in annex.

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Date of the actual completion of the international search

19 May 1994

Date of mailing of the international search report

01.06.94

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Hellemans, W

## INTERNATIONAL SEARCH REPORT

Information on patent family members

Int'l. Application No.

PCT/DK 94/00091

Patent document cited in search report	Publication date	Patent family member(s)		Publication date
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		CA-A-	2054277	16-05-92
		DE-T-	486158	16-12-93
		JP-A-	4289234	14-10-92
DE-A-3334575	05-04-84	CH-A,B	671314	31-08-89
		FR-A,B	2533936	06-04-84
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		JP-A-	59093749	30-05-84
		US-A-	4619703	28-10-86
FR-A-2351152	09-12-77	US-A-	4082887	04-04-78
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		DE-A-	2721725	24-11-77
		GB-A-	1533359	22-11-78
		JP-A-	52140700	24-11-77
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